

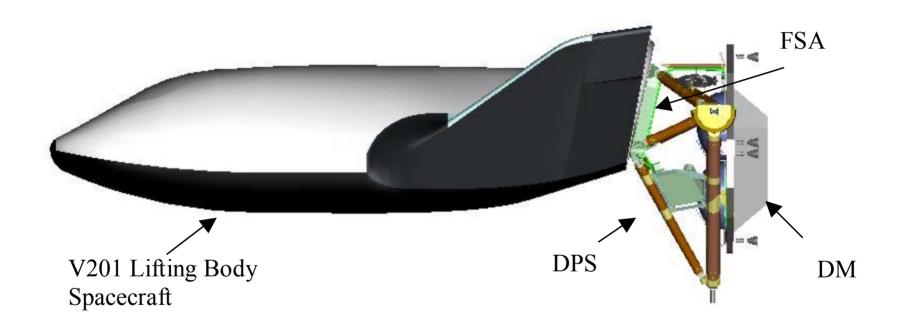
# X-38 De-orbit Propulsion Stage MLI Performance Test

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## Background

- X-38 is Pathfinder for Space Station Crew Return Vehicle
- X-38 Launched in Space Shuttle
- De-Orbit Propulsion System (DPS) Maneuvers X-38 in Descent Trajectory and is Jettisoned Prior to Re-entry
- X-38 DPS design hot biased to reduce power and energy requirements
- Black Beta Cloth selected as outer layer on MLI
- Analytical Margin is Small and no DPS Thermal Testing Planned.



## Objective

- Test DPS MLI
  - Sample Available
  - Test Facilities Available
    - Performed in MSFC Thermal Development Facility
- Determine if MLI Performance Meets or Exceeds that Assumed in Thermal Analyses
- Determine Performance Degradation due to Seams

## Prep Work

- Literature Search of Potential Test Methods
- Test Fixture Conceptual Design
- Thermal Modeling and Analysis
- Design Modification
- Procurement/Manufacturing and Assembly
- Optical Property Measurement
- Instrumentation Acquisition
- Data Acquisition System Setup

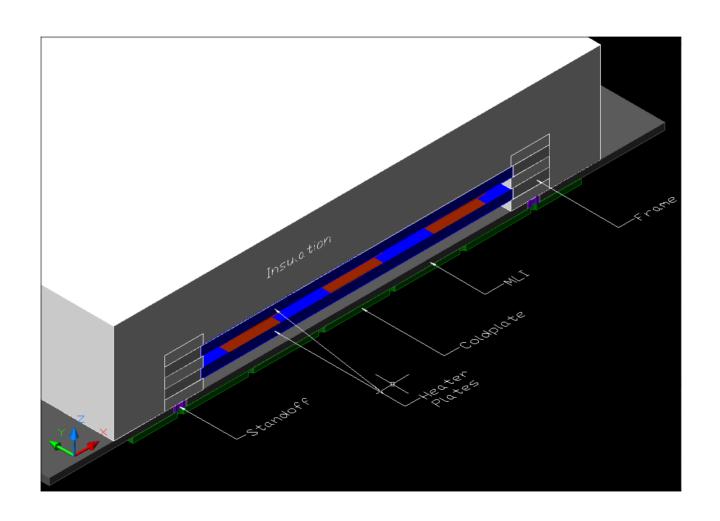
## Initial Test Methodology

- Guarded Heat Flow Technique Loosely Based on ASTM-177-97
- Use Temperature Difference Between Primary Heater Plate and Coldplate, Measured Emissivity for the Primary Heater and MLI, and the Primary Heater Power Draw to Calculate Effective Emittance ( $\varepsilon^*$ )
- Black Anodized Aluminum Heater Plate,  $\varepsilon = 0.83$
- MLI Black Beta Cloth Outer Surface,  $\varepsilon = 0.87$ ,  $\alpha = 0.96$

#### Test Fixture

- Test Fixture Composed of Polysulfone Plastic Frame and two Black Anodized Aluminum Heater Plates
- Mounted to Space Station –1 Coldplate with Teflon Isolators
- Insulated with four inches of Cryolite Fiberglass Matte
- MLI Sandwiched in Interface Between Heater Plates and Coldplate
- One Square Foot Test Area

## **Test Fixture Cross-Section**



## Test Setup

- 9 Minco Thermofoil Heaters per Heater Plate
- Temperature Sensors Mounted on Heater Plates, Coldplate, Frame, and Chamber Shell
- Fixture Isolated from Coldplate with Teflon Standoffs
- MLI Between Test Fixture and Coldplate
- Vacuum Chamber
- Johns Manville Cryo-lite Fiberglass Insulation
- ISS –1 Coldplate and Neslab Low Temperature Chiller
- Residual Gas Analyzer
- DAQ System and Power Supplies

# Test Setup



## Test Setup



#### Test Procedure

- Assemble MLI, Test Fixture, Insulation, and Coldplate in Vacuum Chamber
- Evacuate Chamber Control Heaters to 300°F, Chiller set to 5°F.
- Adjust Heater Power so that Heater Plates are at the Same Temperature
- Record Primary Heater Plate Temperatures and Voltage and Current and Coldplate Temperature

#### **Modifications**

- Heater Plate Thermocouples Replaced with RTD's wired to HP DAQ System
- RTD's Bonded to the Heater Plates using Conductive Epoxy
- Fixture Re-oriented on Coldplate so the Open End was to the Left Rather than Top
- Aluminized Kapton Tape Applied to Fixture Exterior

#### Retest

- Reconfigured Test Yielded more Uniform Temperatures
- Primary Heater Temperature of 297°F and Coldplate Temperature of 12°F yielded  $\varepsilon$ \* of 0.028 based on full heat load of 13.0 btu/hr across MLI
- $\varepsilon^*$  of 0.016 0.019 used in DPS Thermal Analyses.
- Assessment of Test Results Indicates much more Heat Leak from Test Fixture than Expected Causing Over-Estimation of  $\varepsilon^*$

## Reconfiguration for Seam Test

- Removed MLI from Test Fixture and Quartered it.
- Each Piece was then Reversed and laid out so the Seams of Adjacent Pieces Overlap then Taped in Place
- 8 RTD's added to MLI side of Test Fixture Frame.
- Configuration then Reassembled.

# MLI Configuration for Seam Test



#### Seam Test

- Primary Heater Temperature of 295°F and Coldplate Temperature of 22.1°F yielded  $\varepsilon$ \* of 0.044 based on full Heat Load of 19.1 btu/hr across MLI
- Assessment of Test Results Indicates much more Heat Leak from Test Fixture than Expected Causing Over-Estimation of  $\varepsilon^*$
- Frame Temperatures of 235°F Appreciable Higher than Expected

## Post-Test Analysis

- Updated Thermal Model to as-Tested Configuration
- Identified Modeling Assumptions that Might Affect Results
  - Insulation k and Thickness
  - Heater Plate to Frame Heat Transfer
  - Frame (Polysulfone) k
  - Contact Conductance, Heater Plates to Frame and Frame to Frame
- Varied each Parameter to Determine Sensitivity
  - Results Insensitive to Frame k, Contact Conductance
- Looked for Combination that Matched Test Results
  - Apparently only 1
  - Insulation G \* 3.8 Plate to Frame G \* 0.49
- Seam Test  $\varepsilon$ \* = 0.026 MLI Test  $\varepsilon$ \* = 0.011

## Error Analysis

- Look at Analysis Uncertainty due to Potential Instrumentation Errors
  - Assess Potential Errors due to RTD's, Thermocouples, Voltage & Current Measurements and DAQ System
- Rerun Model Correlation with each Error Applied in Both
  + and Directions and Determine Effect on ε\* Prediction
  - Primary Heater Plate Temperature, +/- 0.828°F
  - Guard Heater Plate Temperature, +/- 0.828°F
  - Frame Temperatures, +/- 0.828°F
  - Coldplate Temperature, +/- 2.7°F
  - Chamber Temperature, +/- 2.7°F
  - Heater Voltage, +/-(0.0003V+0.012) volts
  - Heater Current, +/-(0.002I+0.00025) amps

#### Results

- The Expected  $\varepsilon^*$  Range was Computed by Taking the Square Root of the Sum of the Squares of the Variances Induced by the Potential Error Cases and Applying those to the Nominal Values
  - Seam Test  $\varepsilon^* = 0.017 0.035$
  - MLI Test  $\varepsilon$  \* = 0.003 0.019
- Assuming the Overlapped Seams Affect an Area 0.5" Wide and the Remainder of the Area in the Seam Test has the same  $\varepsilon^*$  as Computed for the MLI Test, an  $\varepsilon^*$  for just the Seam Area was Computed
  - $\varepsilon$  \* = 0.175 0.215
  - This Value can be Combined with the  $\varepsilon^*$  from the MLI Test in an Area Weighted Manner to Estimate the Overall Performance of the X-38 MLI Blanket System.

#### Lessons Learned/Conclusions

- It's Difficult to Effectively Insulate an Effective Insulator
- Polysulfone is Easily Machinable, Vacuum Stable, and has a Good Temperature Range (-150°F to +350°F)
- Cryolite is a Fiberglass Matte Insulation with a Vacuum Stable Melamine Resin, Rated for -450°F to +450°F
  - It does have Quite an Affinity for Water Vapor.
  - The Thermal Conductivity is Apparently Higher than the Manufacturer's Value.
- A Horizontal Test Setup is much Preferable to Vertical
- A Guard Heater Complicates Model Correlation
- Testing a Larger Sample Area would have Improved Results